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# **QUANTITATIVE TEXTURE ANALYSIS OF BLANKET FILMS AND INTERCONNECTS**

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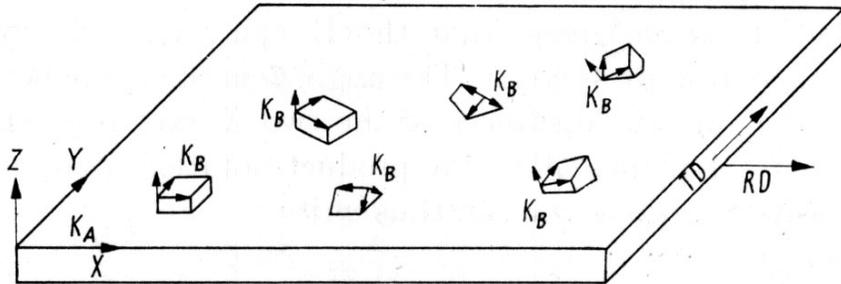


# Outline

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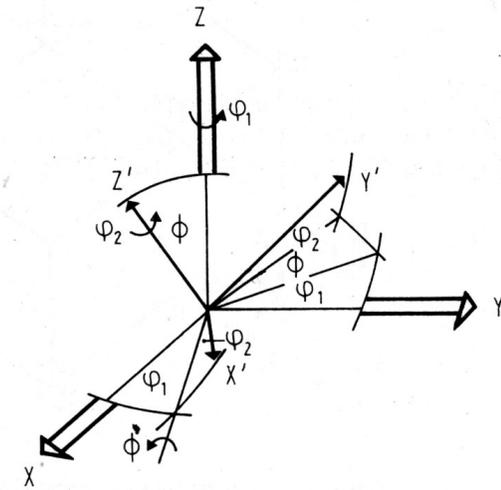
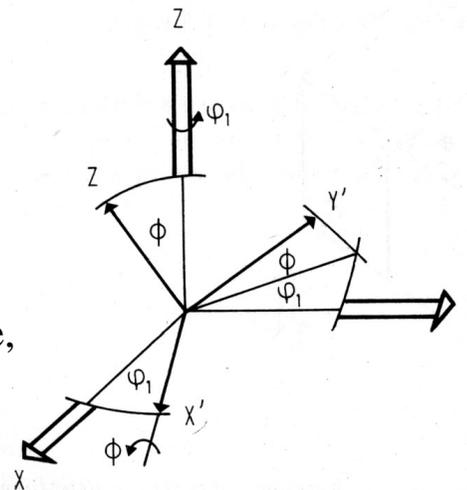
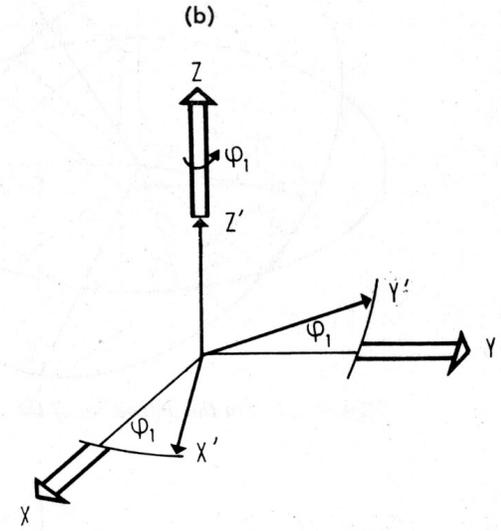
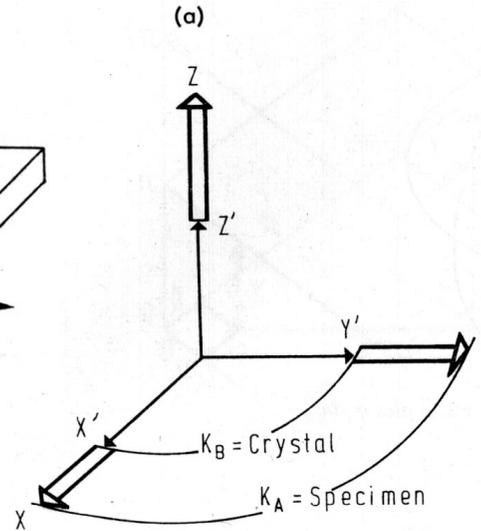
1. Overview QTA: Orientation Distribution Function (ODF)
  - measurement of pole figures,
  - transformations from pole figures to ODF
  - precision and accuracy issues
  - graphical and numerical representation of texture data
  
2. How are texture measurements and analysis in thin film structures different from a traditional approach for bulk materials?
  - experimental requirements and solutions,
  - ODF analysis
  
3. Examples of QTA applied to copper metallization technology.

# Orientation of Individual Crystallites: Definition of Euler Angles



$$g : [K_A \rightarrow K_B)$$

$$g \equiv (\varphi_1, \phi, \varphi_2)$$



H.J. Bunge, Texture Analysis in Materials Science,  
(Butterworths, London, 1982)

# Rotation $g$ Defines Crystal Orientation

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- $g$  may be specified in numerous ways:
  - $g=[g_{ij}]$  orientation matrix 9 parameters
  - $g=\{\nu\psi\omega\}$  axis-rotation angle 3 parameters
  - $g=(hkl)[uvw]$  metallurgical 6 parameters
  - $g=\{\phi_1\Phi\phi_2\}$  Euler angles 3 parameters
- Several variants of Euler angles are in use:
  - $\{\phi_1\Phi\phi_2\}$  H.-J. Bunge, *Texture Analysis in Materials Science*, Butterworths, London, 1982.
  - $\{\Psi\Theta\Phi\}$  R. J. Roe, *J. Appl. Phys.* **36** (1965) 2024-2031.
  - $\{\alpha\beta\gamma\}$  S. Matthies, G. W. Vinel, K. Helming, *Standard Distributions in Texture Analysis*, Akademie, Berlin, 1987.



# Orientation Distribution Function $f(g)$ : Definition of Texture

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Orientation distribution by volume:

$$\frac{dV}{V} = f(g)dg$$

Where:  $dV$  is the volume of crystallites that have the orientation  $g$  within the element of orientation  $dg$ , and  $V$  is the total sample volume.

Orientation distribution by number of crystallites:

$$\frac{dN}{N} = n(g)dg$$

$$dg = \frac{1}{8\pi^2} \sin \Phi d\varphi_1 d\Phi d\varphi_2$$



# Experimental Methods of Texture Measurement

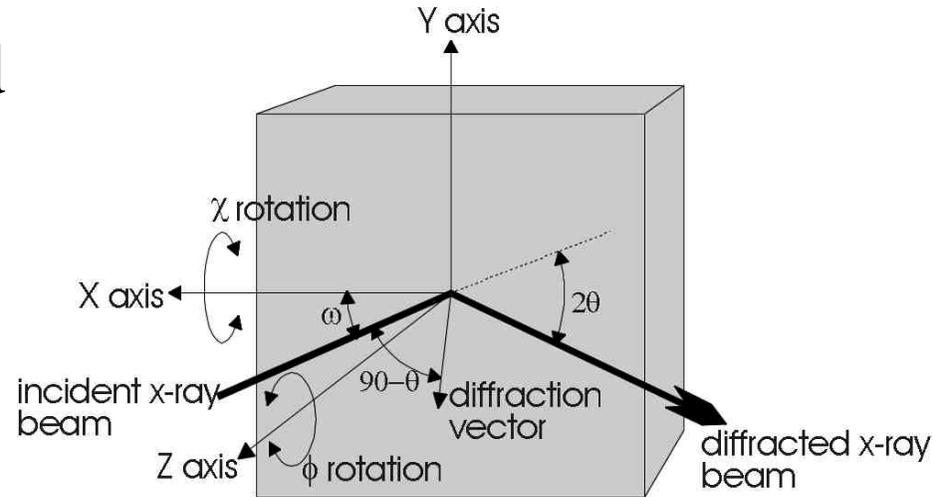
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- Individual orientation measurement:  $g_i$  and corresponding  $V_i$  of all crystallites in the sample, construction of  $n(g)$  or  $f(g)$ .
- **Pole figure measurement**: direct measurement of  $dN$  or  $dV$  of crystallites with two angular parameters fixed and the third varied through all possible values, calculation of ODF from several pole figures.
- Indirect calculation of ODF from measurement of anisotropy of physical properties (elastic, magnetic, electrical).

# Pole Figure Measurements by Diffraction Methods

## Fixed diffraction vector method

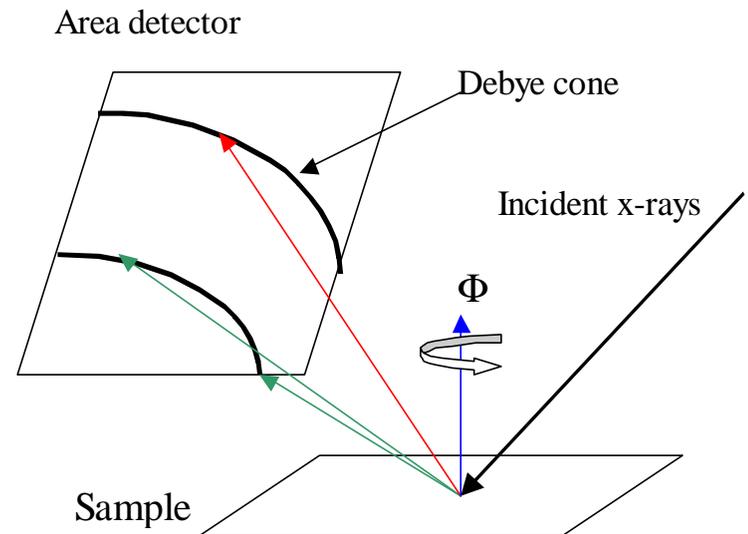
Need at least two independent rotations (e.g.  $\Phi$  and  $\chi$ ) but usually texture goniometers allow three sample rotations ( $\Phi$ ,  $\omega$  and  $\chi$ )



## Variable diffraction vector method

Diffraction vector varies along Debye ring and for different Debye rings

Only one sample rotation angle is needed ( $\Phi$ )





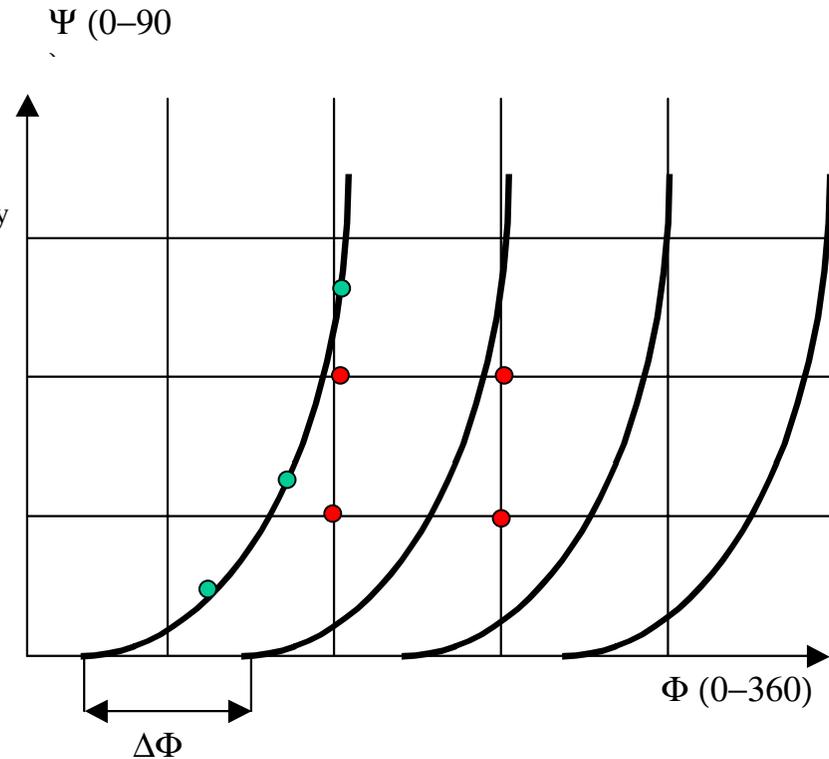
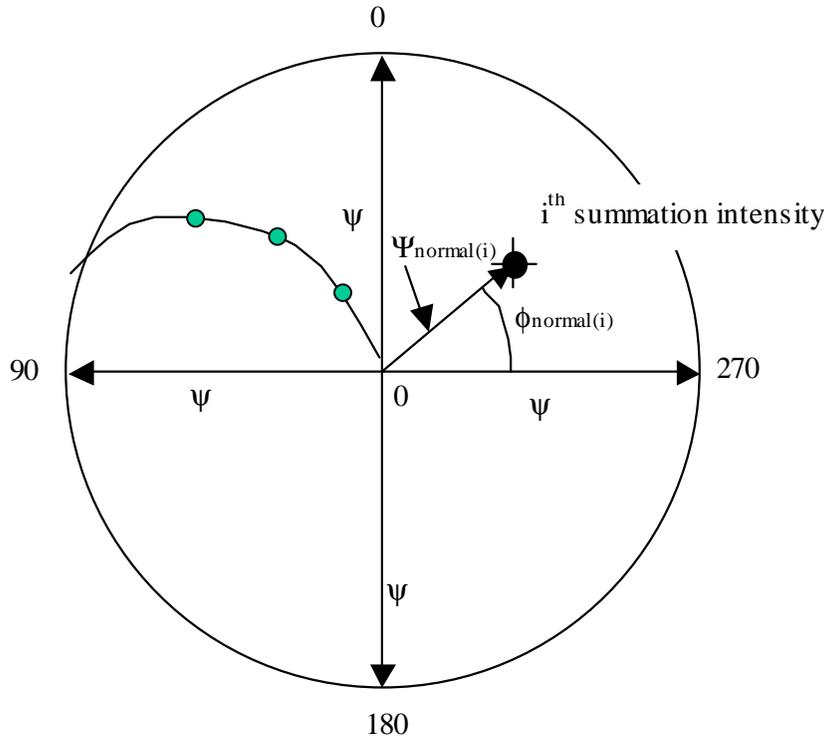
# Intensity Distributions Are Not Pole Figures

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- **Intensity to pole density conversions include:**
  - Absorption corrections (necessary for tilts  $>70$  degrees)
  - Defocusing corrections
  - Background corrections
  - Variable diffracting volume (especially for thin films)
- **Corrections in pole figure space:**
  - Sample misalignment
  - Parallax errors (detector space)
  - Interpolation in pole figure space
  - Pole figure normalization
- **Goniometer misalignment errors are generally not correctable (e.g. peak shifts with tilt, etc.)**
- **Individual pole figures and sets of pole figures must be self-consistent**



# Asymmetric Diffraction Geometry Results in Non-Equidistant Mapping in Pole Figure Space



All ODF programs accept pole figure data on a equidistant mesh

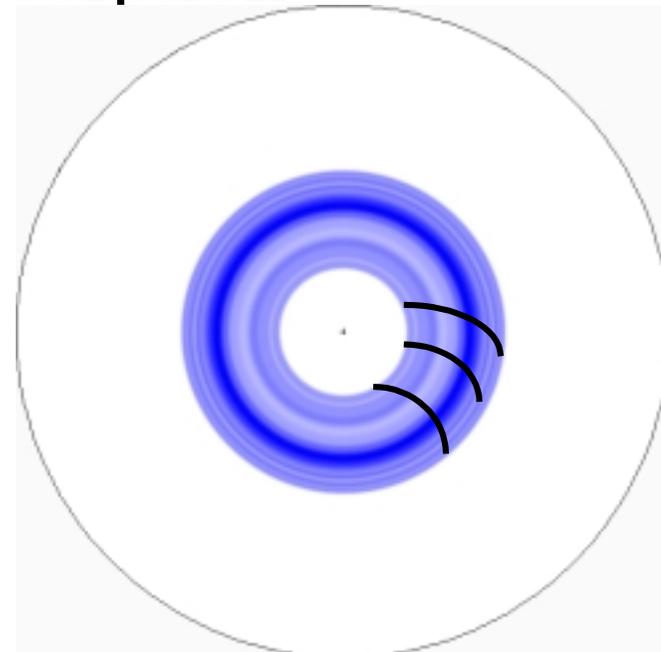
Interpolation in PF space is necessary

Angular resolution of PF's must match the sharpness of measured texture

# Thin Films: Experimental Specifics

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- Finite thickness often requires grazing incident geometry (asymmetric diffraction)
- Tilt dependent (varying) penetration depth may hinder analysis but can be controlled
- Multilayers require additional absorption correction
- Diffracting volume changes with tilt
- Experiments always result in incomplete pole figures





# Pole Figure Inversion Methods

Method	Source Codes	Resolution	Solution (texture dependent)	Computer Time
<i>Fourier Methods</i>				
Classical harmonic	Many available; e.g., Jura et al., 1976	} Limited by L  Residual error	$\tilde{f}(g)$	1*
Zero range	Bunge-Esling		} weak tex.: $\tilde{f}(g)$	5
Iterative positivity	Dahms-Bunge			3
Quadratic form	Van Houtte		} strong tex.: $f(g)$	10
Maximum entropy	Liang et al.		Smooth ODF	
<i>Direct Methods</i>				
Vector	Vadon, Schaeben	} Limited by computer	} weak tex.: $\tilde{f}(g)$	10
Imhof	Imhof			5
Pawlik-Pospiech	Pawlik, Pospiech	} Good	} strong tex.: $f(g)$	1
WIMV	Matthies-Vinel, Kallend			Smooth with strong peaks
<i>Gauss correction</i>	Lücke, Pospiech	Residual error	Strong peaks	

# Error Criteria for ODF Calculations

$$RP(\varepsilon) = \frac{1}{IJ} \sum_{i=1}^I \sum_{j=1}^J \frac{|PF_{ij}^{cal} - PF_{ij}^{exp}|}{PF_{ij}^{exp}} \theta(\varepsilon, PF_{ij}^{exp}) 100\%$$

$$\theta(\varepsilon, x) = \begin{cases} 0 & \text{for } x \leq \varepsilon \\ 1 & \text{for } x > \varepsilon \end{cases}$$

where: i indicates the pole figure, I is the number of pole figures taken for ODF calculation, j indicates a point on a pole figure and J is the number of points on the pole figure taken for ODF calculation

**Table 2. RP error measures (practical experience, Wenk and Matthies)**

RP %	Maximum deviations expected in pole figures $\pm$ m.r.d.	Applicability
0.5 - 1	0.05	Resolution of most methods
1 - 2	0.1	Excellent experimental pole figures
2 - 5	0.2	Good pole figures—weak textures
5 - 10	0.5	Good pole figures—strong textures
> 10	1.0	Problems with data

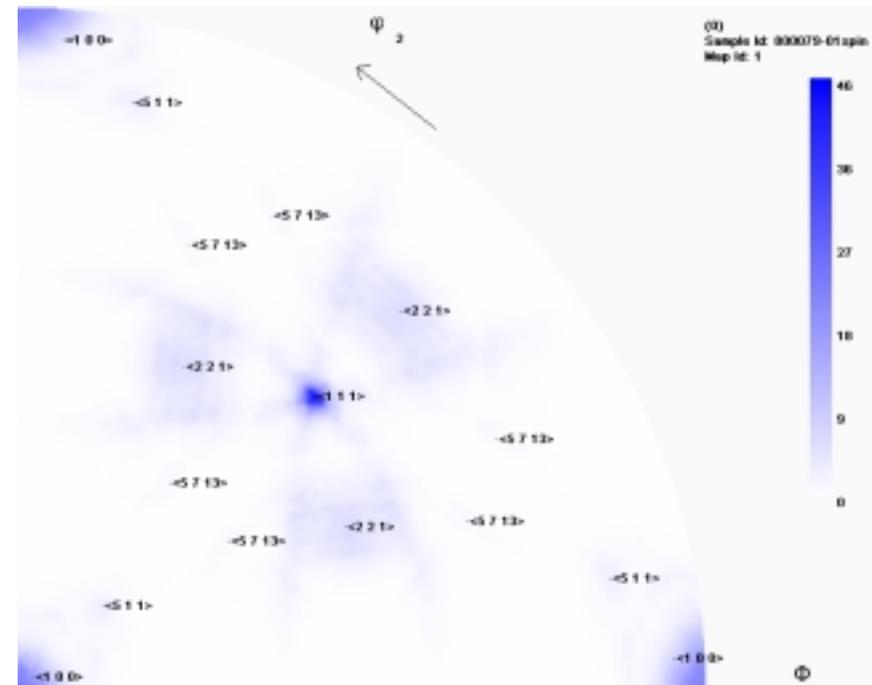
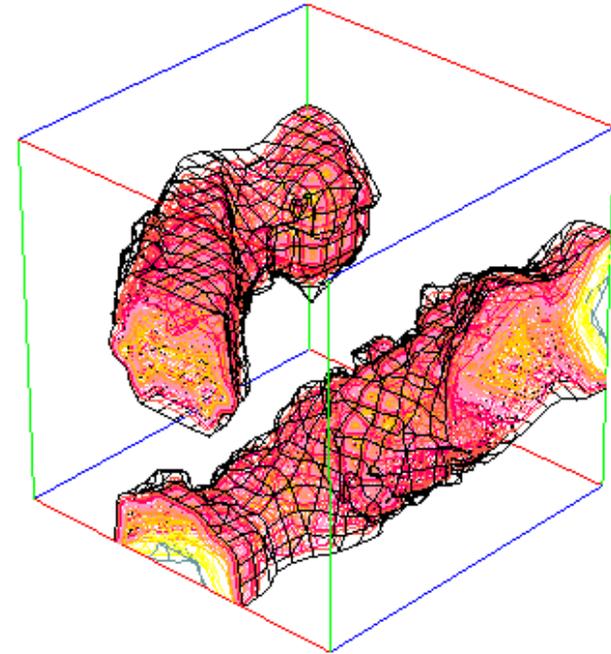
# Representations of ODF

For cubic-orthorhombic symmetry ODF with 1 deg. resolution contains 729,000 values

Graphic representations are semi-quantitative and include:

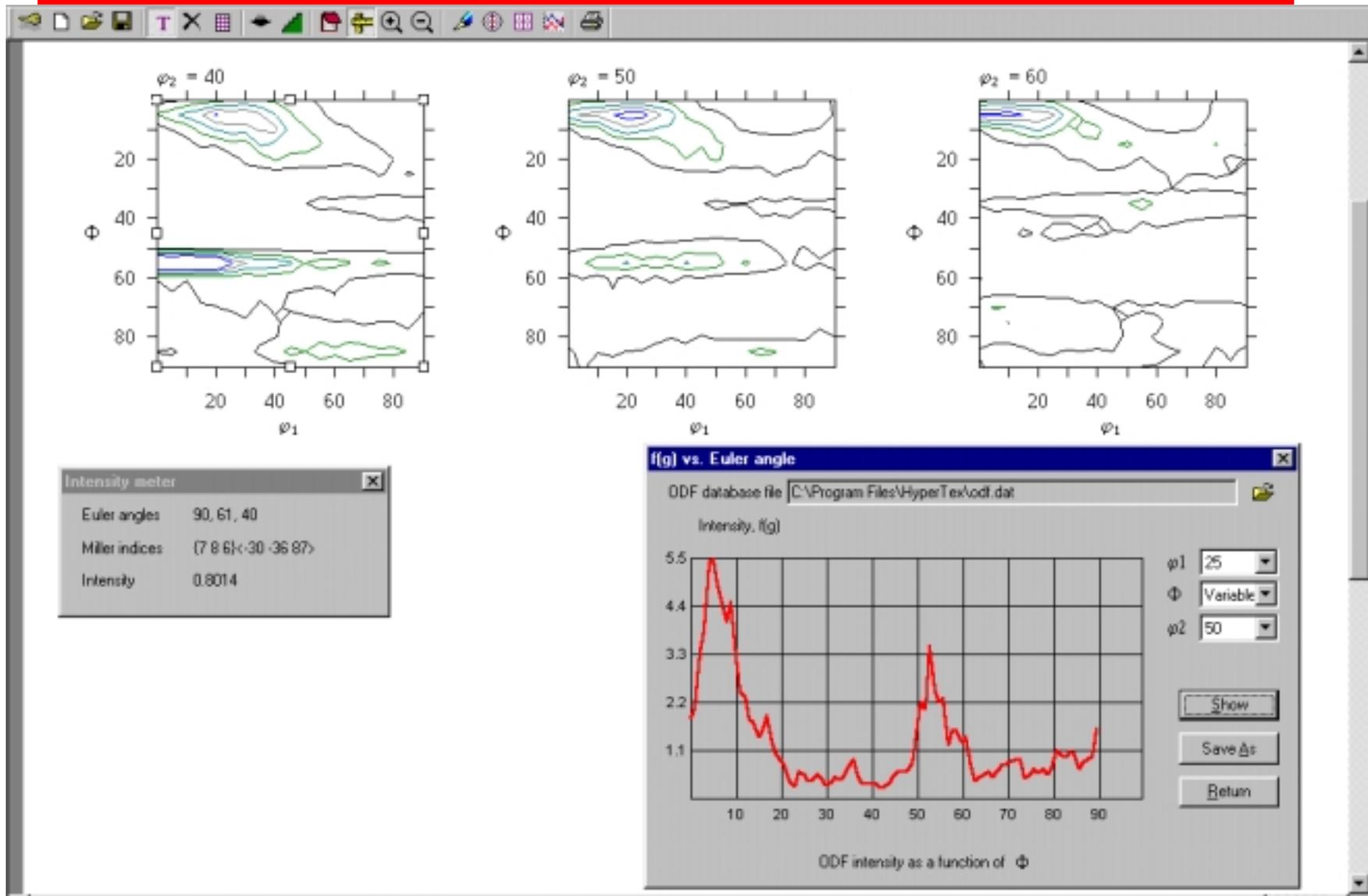
- 3-D cross-sections
- 2-D cross-sections
- Cartesian or polar coordinates

Quantitative representation by model functions (texture components)





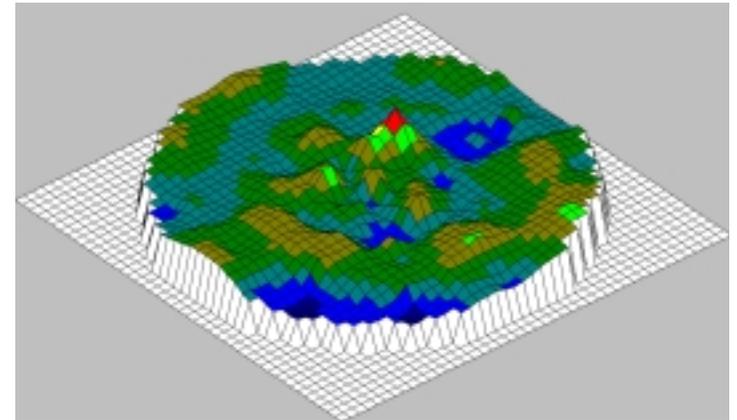
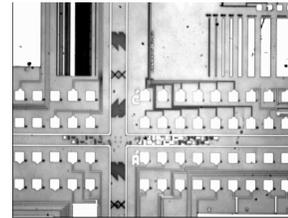
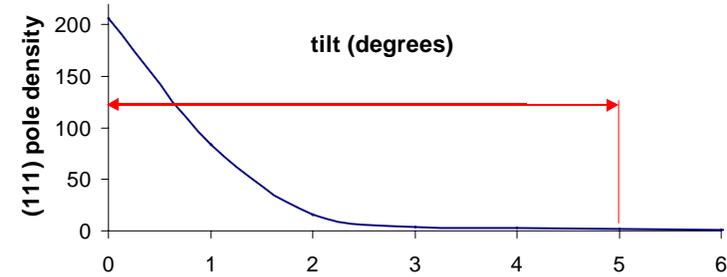
# Representation of ODF by 2D and 1D Cross-Sections





# Semiconductor Industry Imposes New Requirements on Texture Analysis

- High resolution texture analysis:
  - High resolution of reciprocal space mapping
  - Direct methods of ODF calculations
- High spatial resolution:
  - Precision in beam and sample positioning
  - Small x-ray beams
  - Stationary sample
- Mapping capability
  - Accommodate 200 and 300 mm wafers

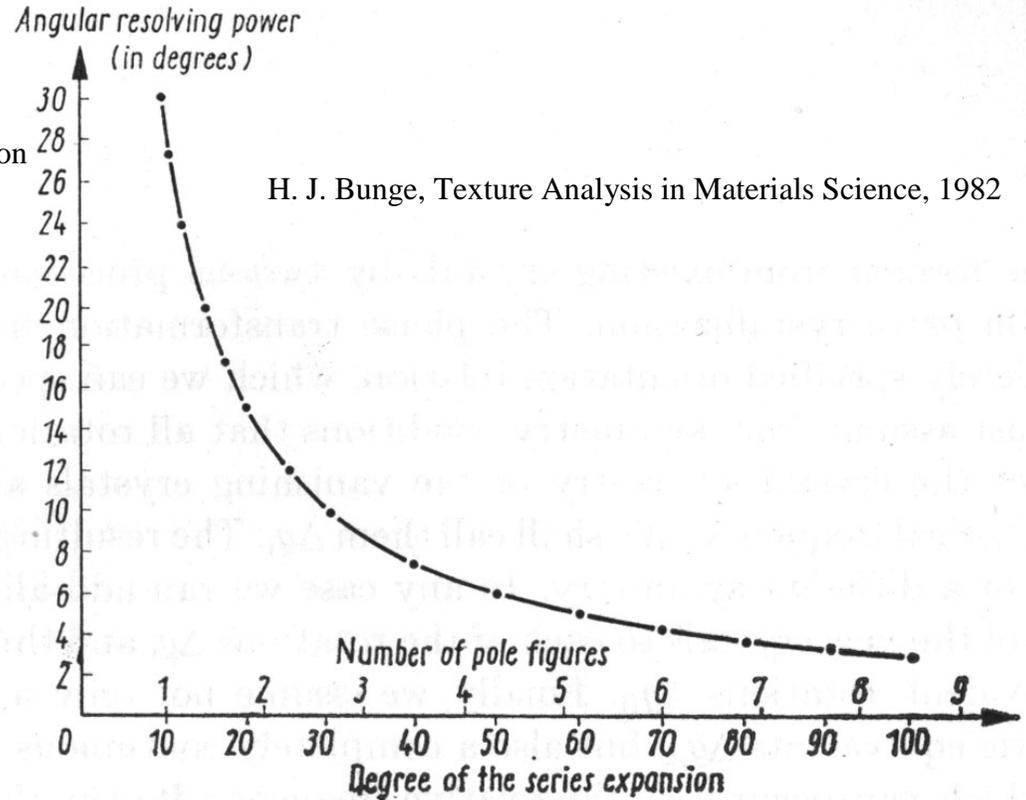
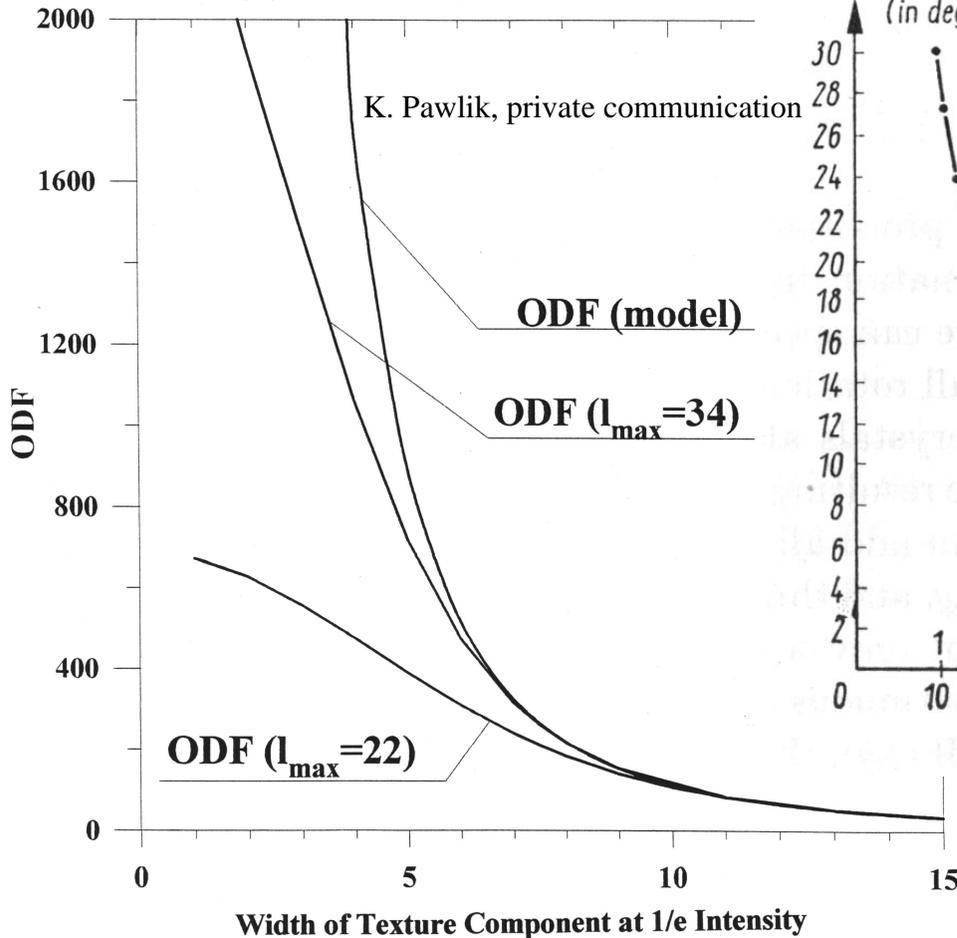


- Other: throughput, contamination control, automation



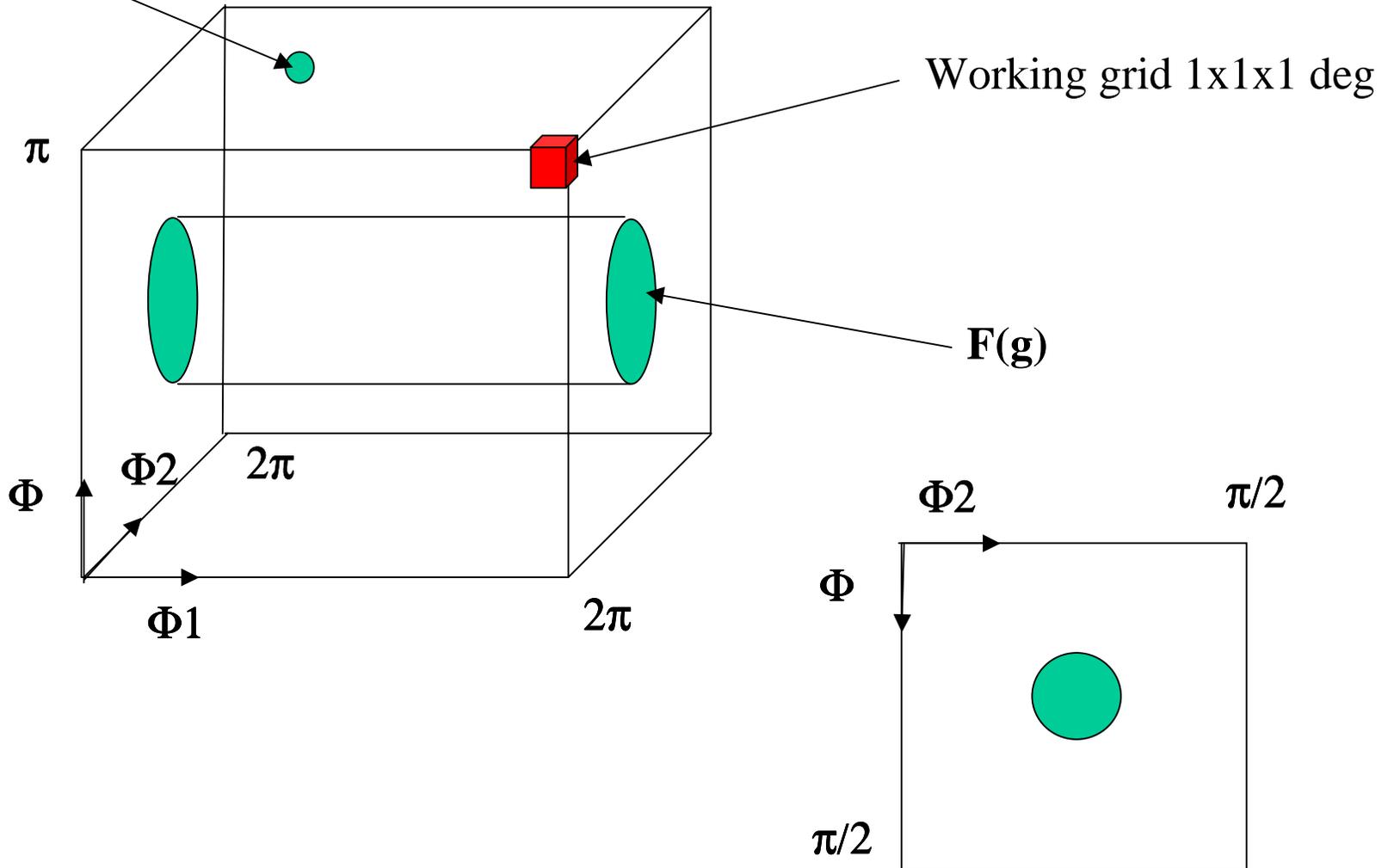
# Methods Based On Series Expansion Lack Resolving Power For Sharp Textures

Effect of the expansion level  $l_{\max}$  (harmonic methods) on the reproduced ODF value



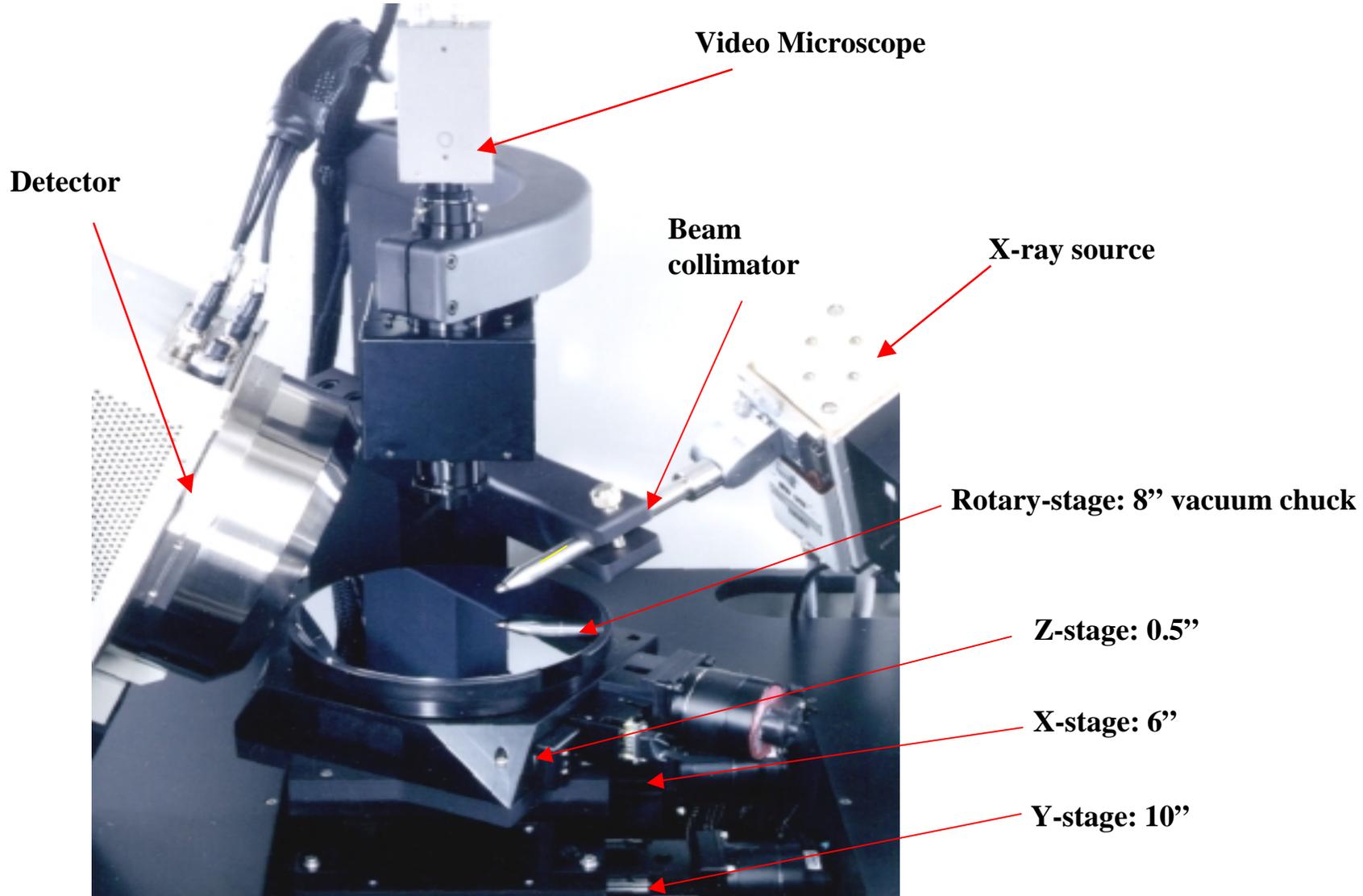
# Direct Methods (WIMV, ADC) With 1 Degree Resolution Are Preferred

Single orientation

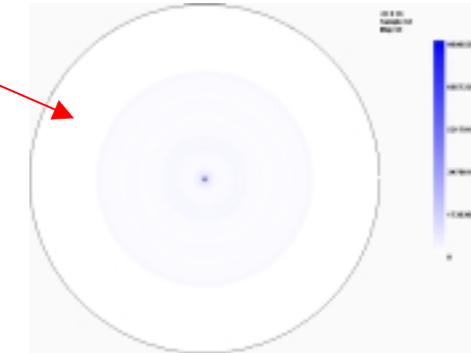
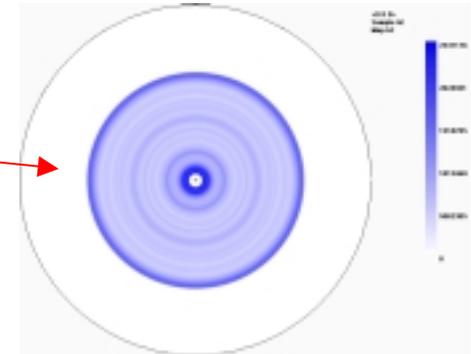
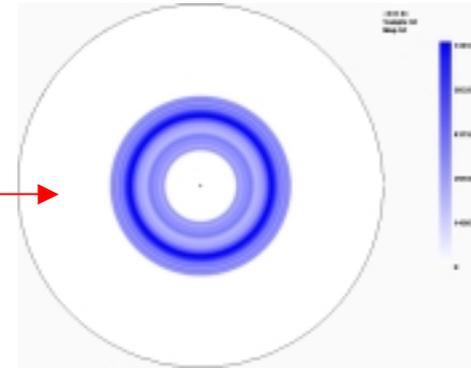
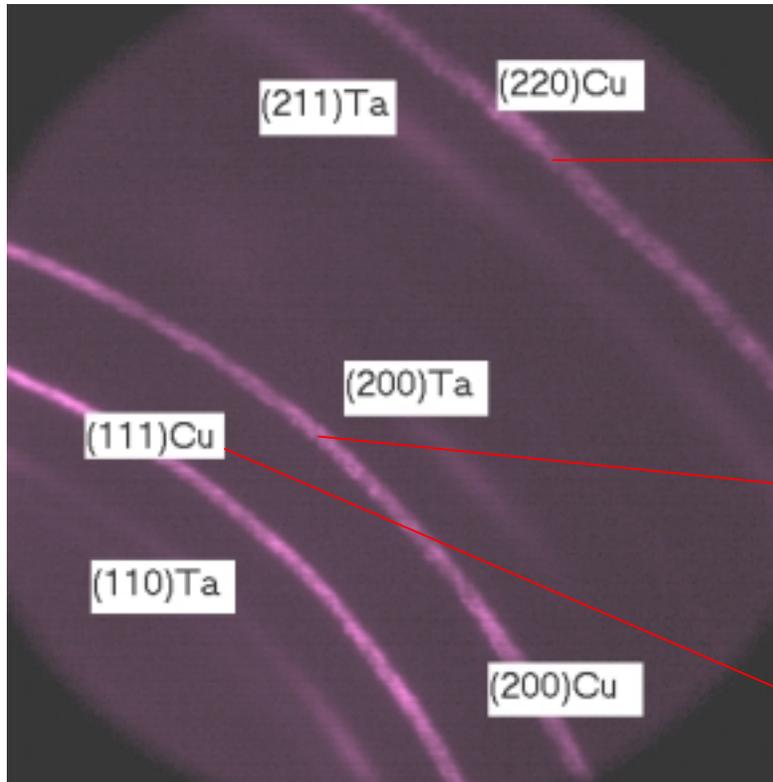




# Measurement Platform of Texture Mapping Instrument



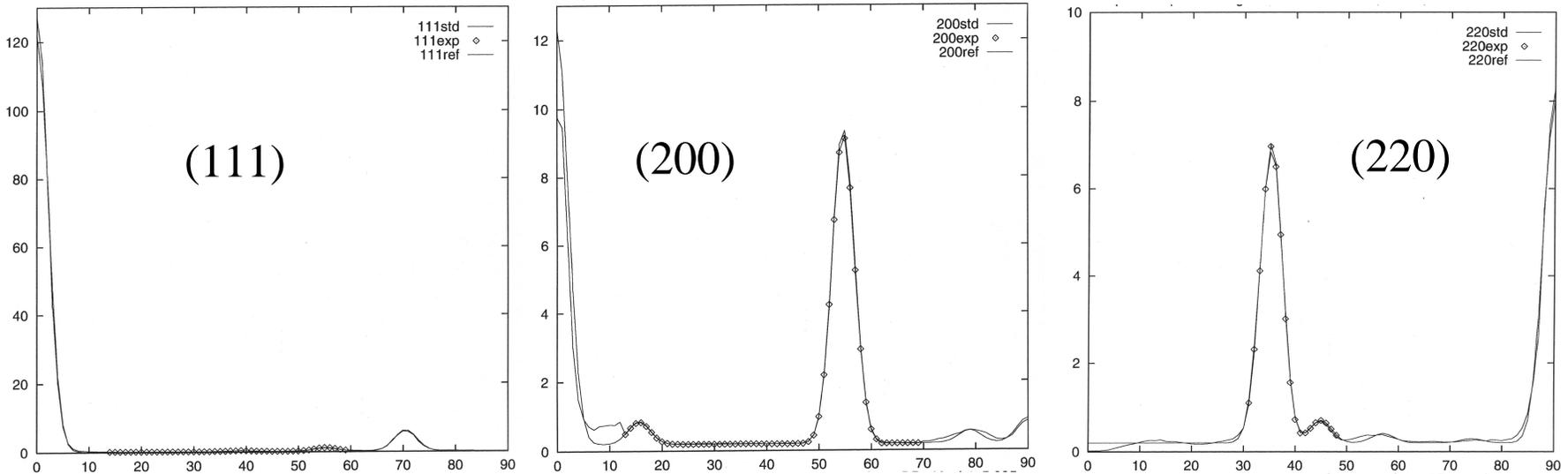
# Several Incomplete Pole Figures Are Measured Simultaneously



Debye rings registered on detector face  
0.5 micron electroplated copper deposited on  
300Å thick Ta barrier layer



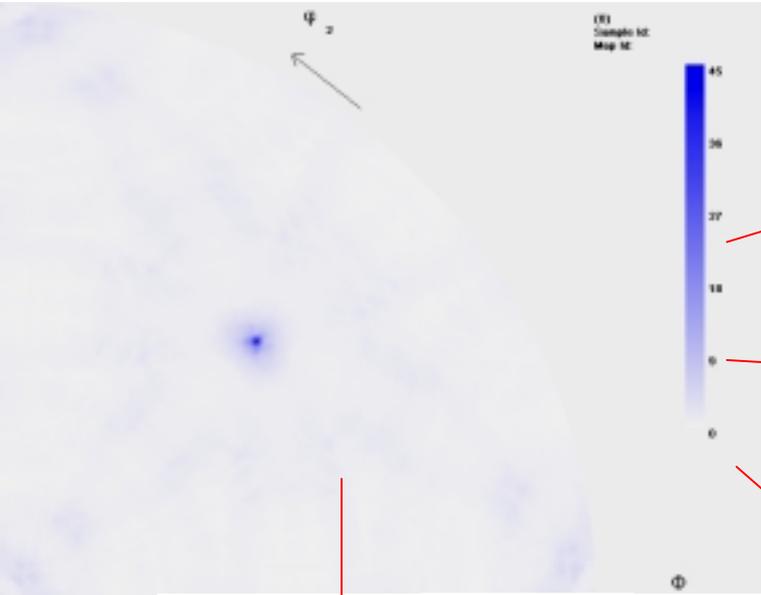
# Pole Figure Ranges Are Optimized For Materials And Textures Typical of Semiconductor Industry



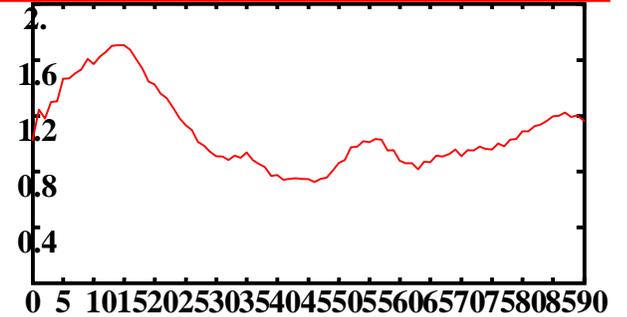
- Use model functions to simulate ODF
- Select ranges on PF satisfying MPDS criterion
- Use partial PF to recalculate ODF
- Estimate relative error (<2%)

$$RP(\varepsilon) = \frac{1}{IJ} \sum_{i=1}^I \sum_{j=1}^J \frac{|PF_{ij}^{cal} - PF_{ij}^{mod}|}{PF_{ij}^{mod}} 100\%$$

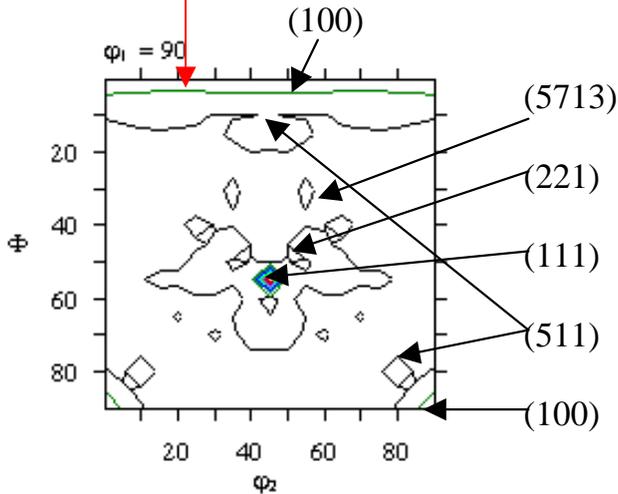
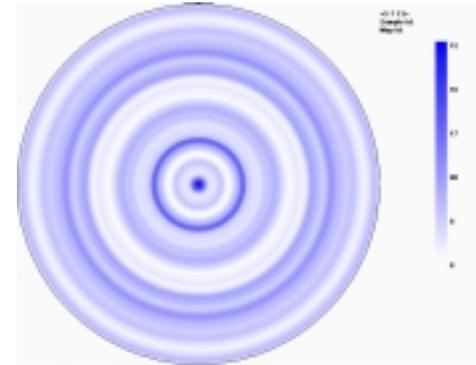
# Quantitative Texture Analysis Offers Numerous Outputs



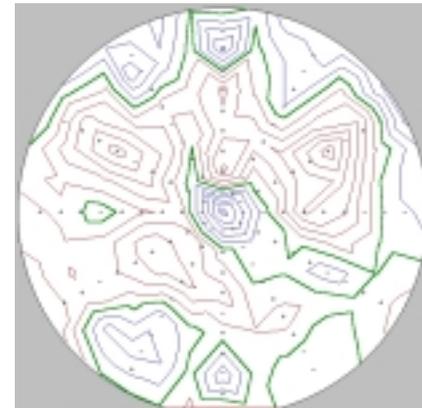
Line plots



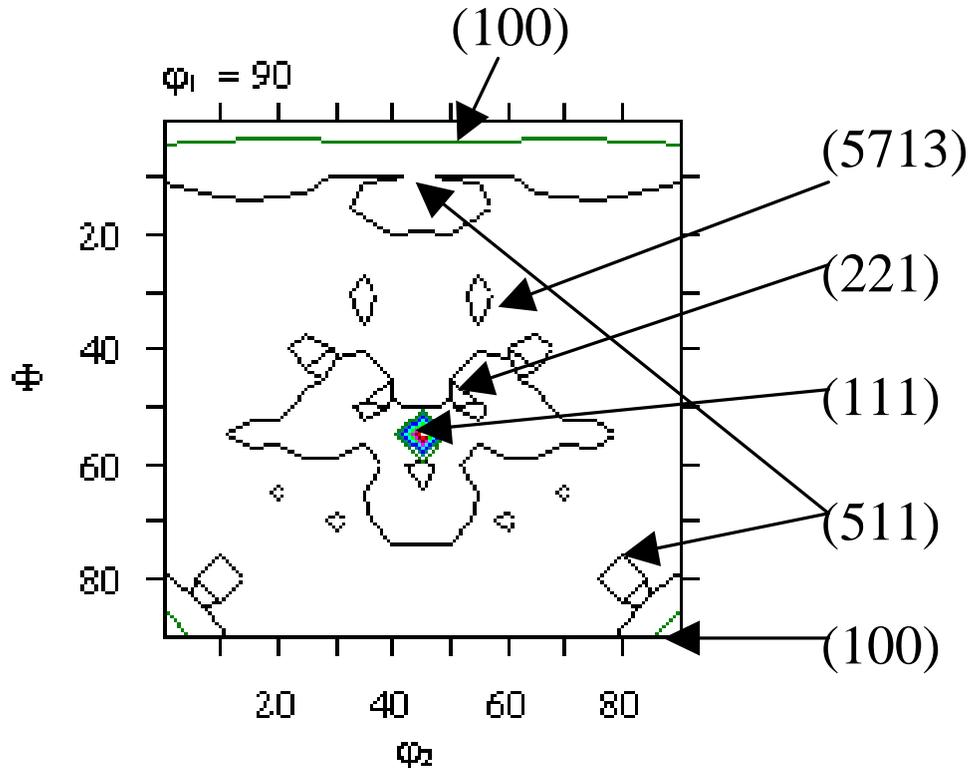
Pole figures



Volume fraction maps



# Volume Fractions of Texture Components Are A Quantitative Measure Easy to Interpret

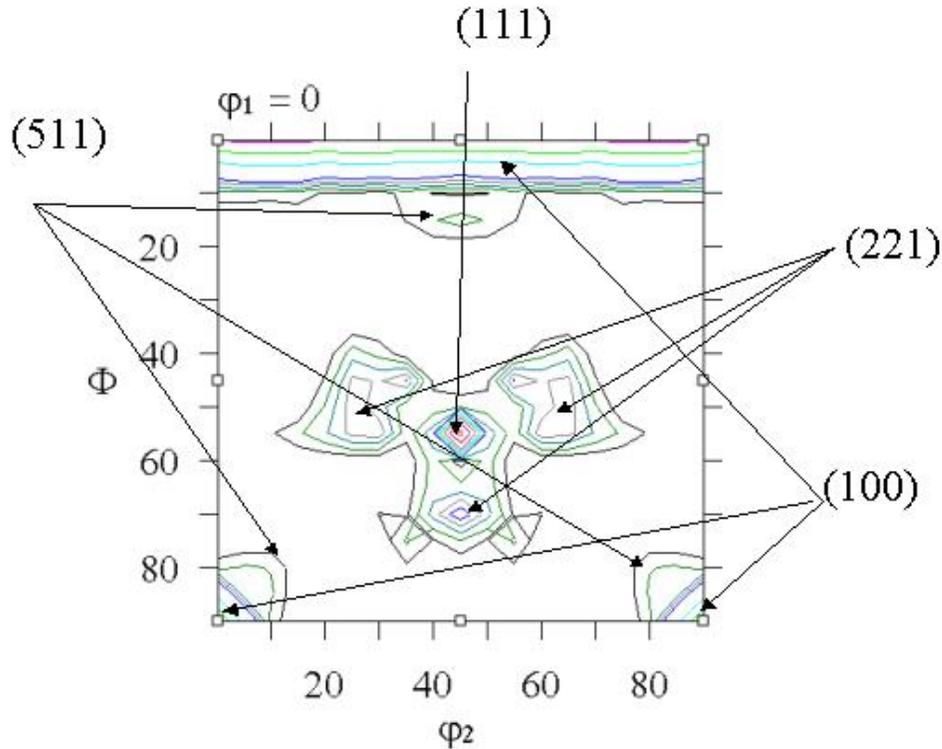


Volume fractions of texture components with cyclic fiber textures are determined with accuracy better than 5% and precision of 0.5%

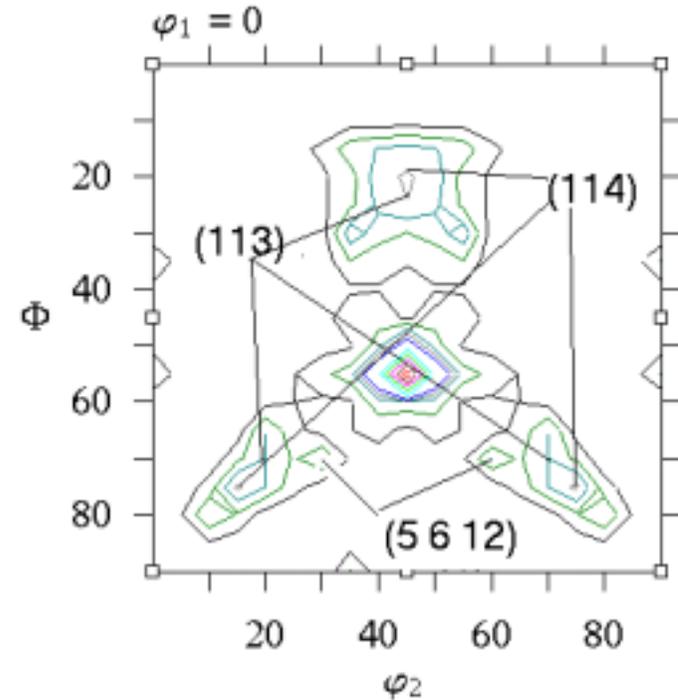
$$\frac{dV}{V} = f(g)dg$$

$$dg = \frac{1}{8\pi^2} \sin \Phi d\phi_1 d\Phi d\phi_2$$

# Errors in Volume Fraction Analysis Are Estimated Using Model Textures



1.0 $\mu\text{m}$  PVD/0.25  $\mu\text{m}$  EP blanket  
copper film annealed at 300C  
for 0.5 hour



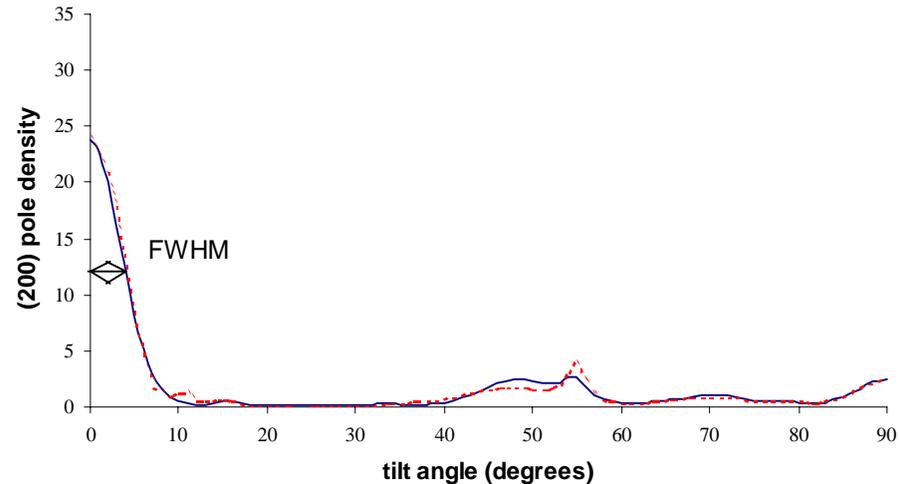
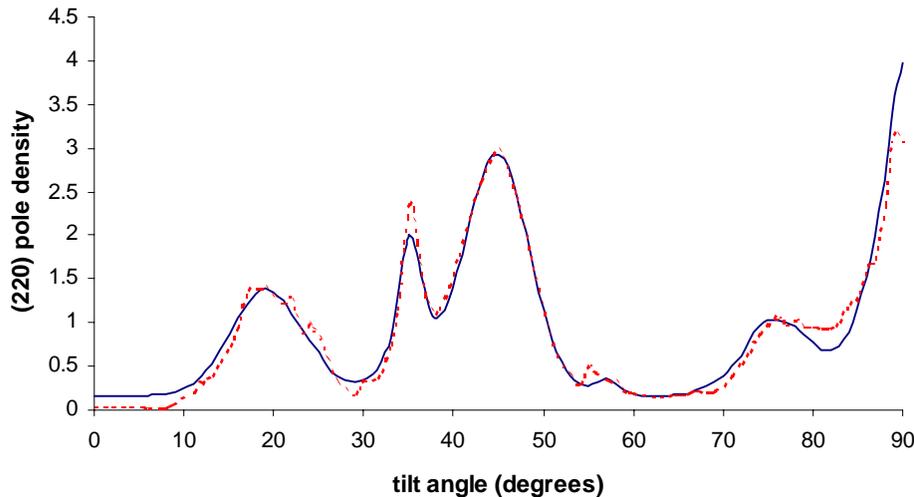
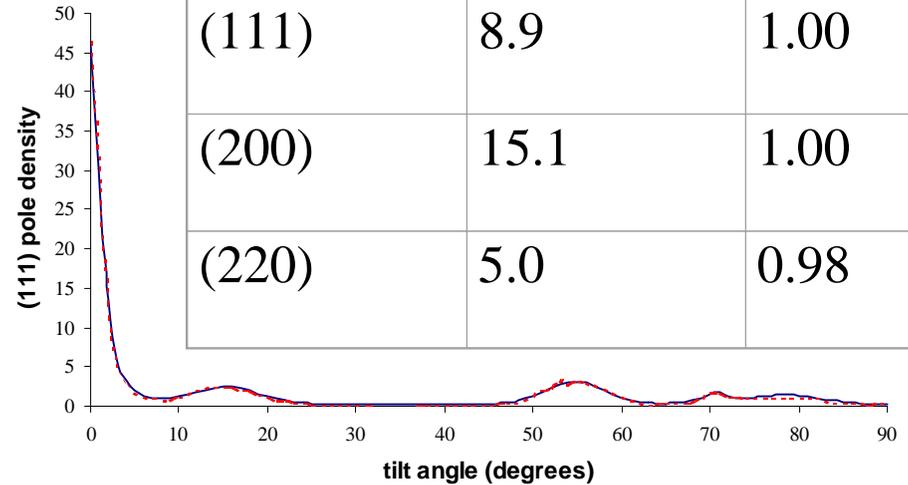
1.0 $\mu\text{m}$  PVD/0.25  $\mu\text{m}$  EP blanket  
copper film recrystallized at room  
temperature



# QTA of 1.0 $\mu\text{m}$ PVD/0.25 $\mu\text{m}$ EP blanket copper film annealed at 300C for 0.5 hour

Texture component	Volume fraction	FWHM (deg)
(111)	0.15	2.5
(511) 1-st gen. twin	0.02	3.0
(5713) 2-nd gen twin	0.01	3.0
(100)	0.25	8.0
(221) 1-st. gen. twin	0.40	9.0
Random	0.15	-

Pole Figure	RP(1) (%)	Correlation
(111)	8.9	1.00
(200)	15.1	1.00
(220)	5.0	0.98

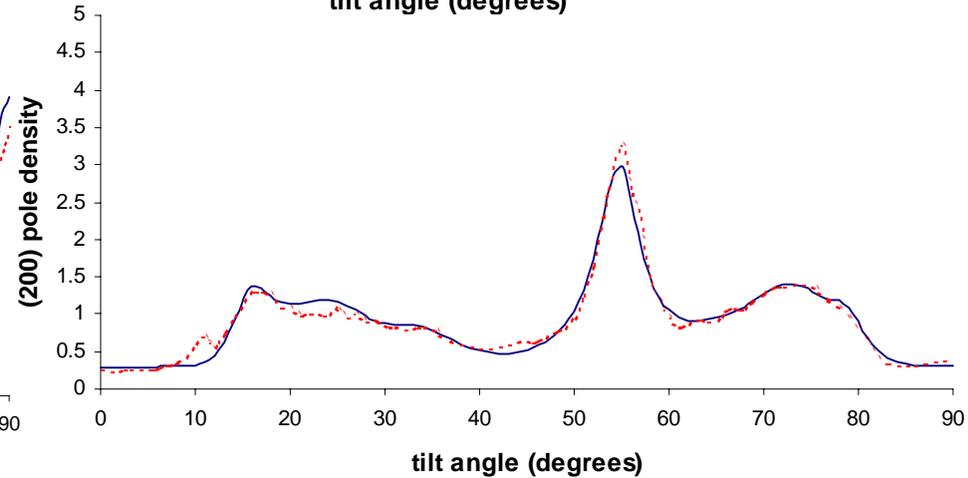
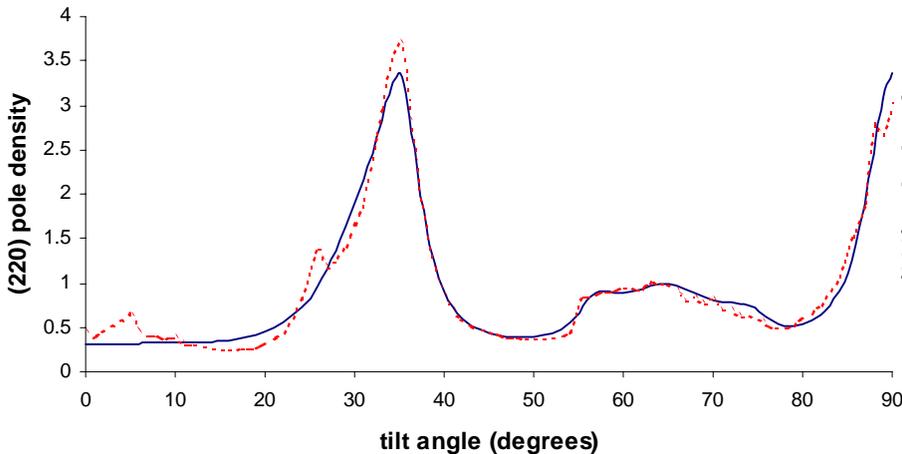
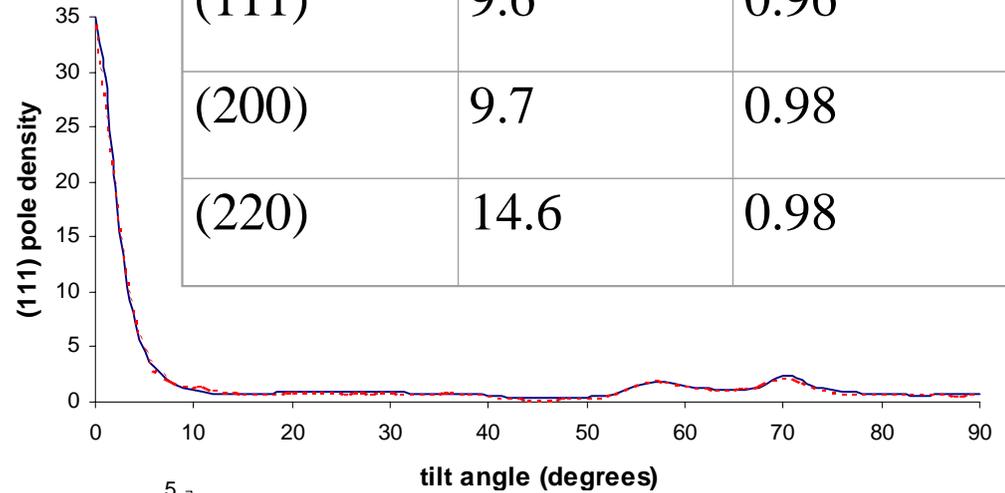




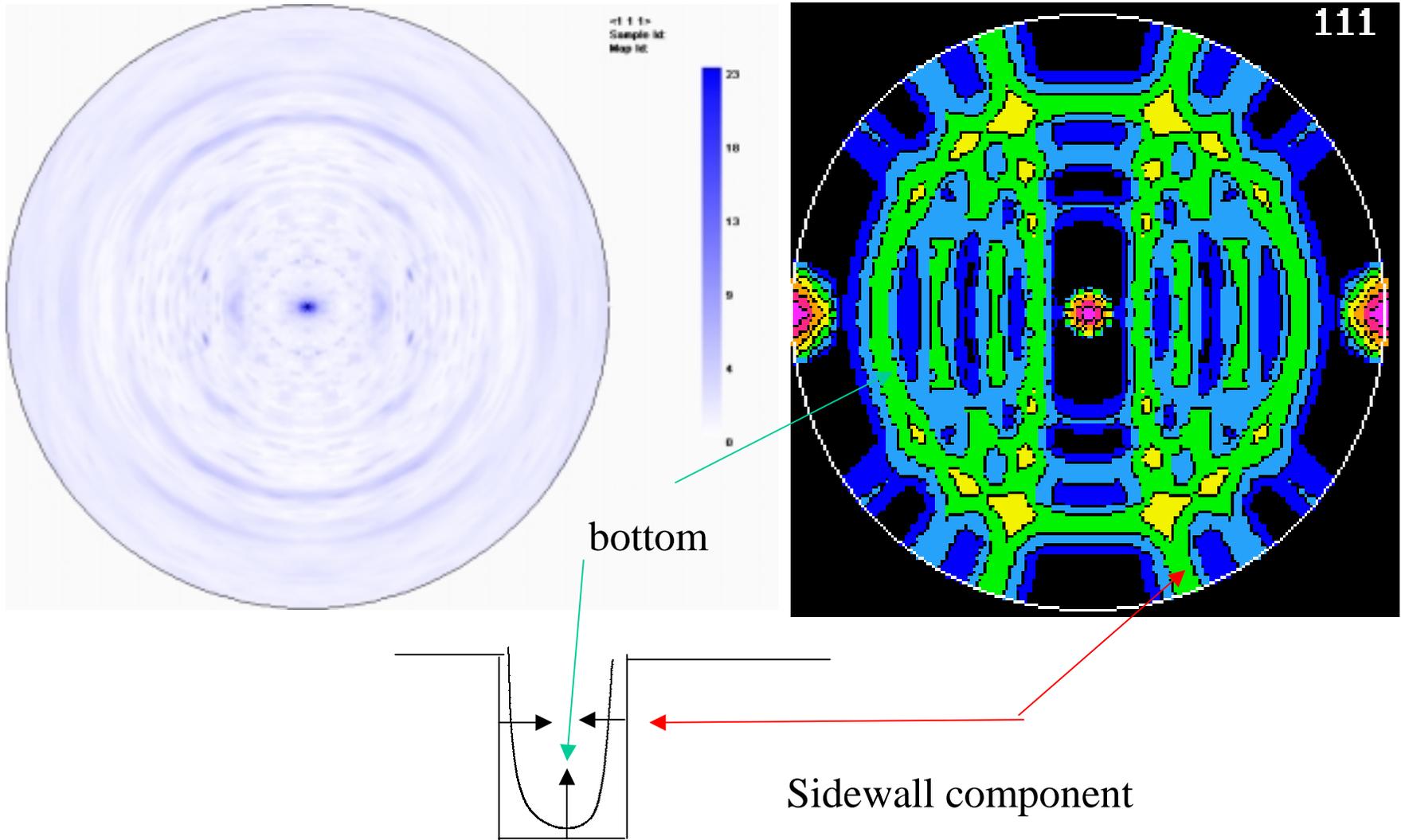
# QTA for 1.0 $\mu\text{m}$ PVD/0.25 $\mu\text{m}$ EP blanket copper film recrystallized at room temperature

(111)	0.34	4.5
(113)	0.10	7.0
(114)	0.10	8.0
(115)	0.04	4.0
(56 12)	0.15	10.0
Random	0.27	-

Pole Figure	RP(0) (%)	Correlation
(111)	9.6	0.96
(200)	9.7	0.98
(220)	14.6	0.98



# Texture Modeling Helps to Interpret Experimental Results





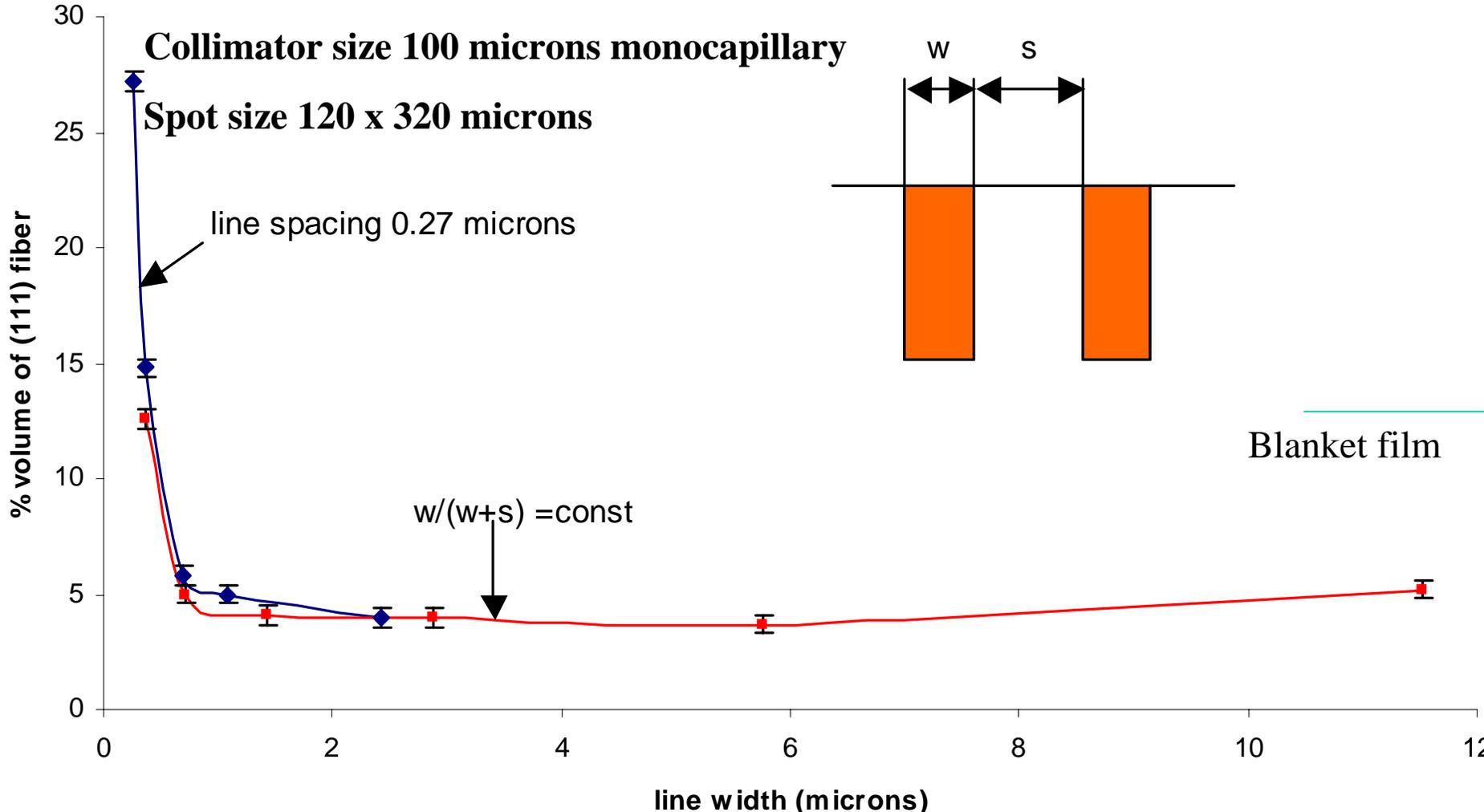
# High Spatial Resolution ( $\sim 100 \mu\text{m}$ ) and Precision In Positioning ( $\sim 10 \mu\text{m}$ ) Is Often Required

Electroplated Damascene Copper +CMP,  
Structure Size  $300 \times 500 \mu\text{m}^2$

Collimator size 100 microns moncapillary

Spot size  $120 \times 320$  microns

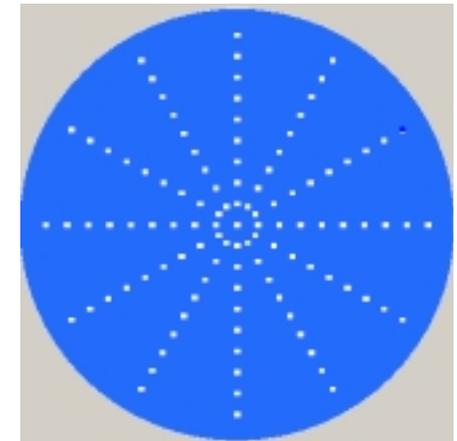
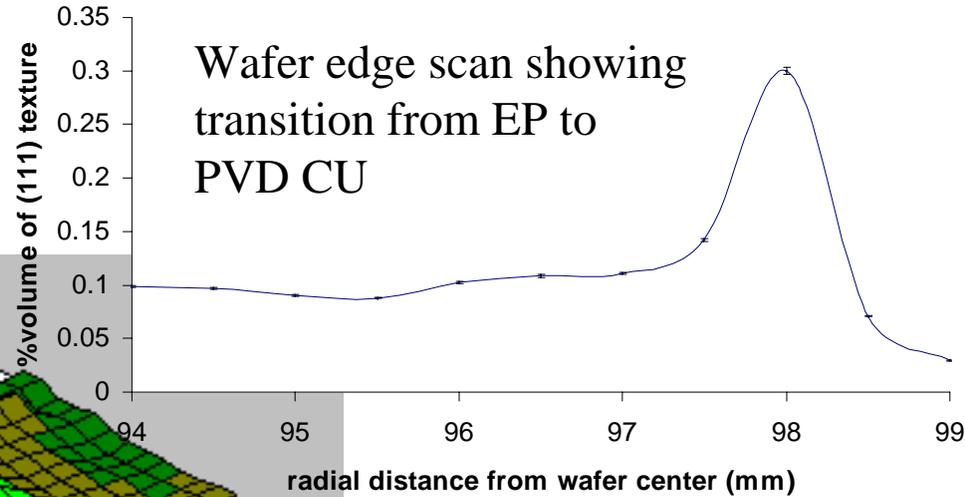
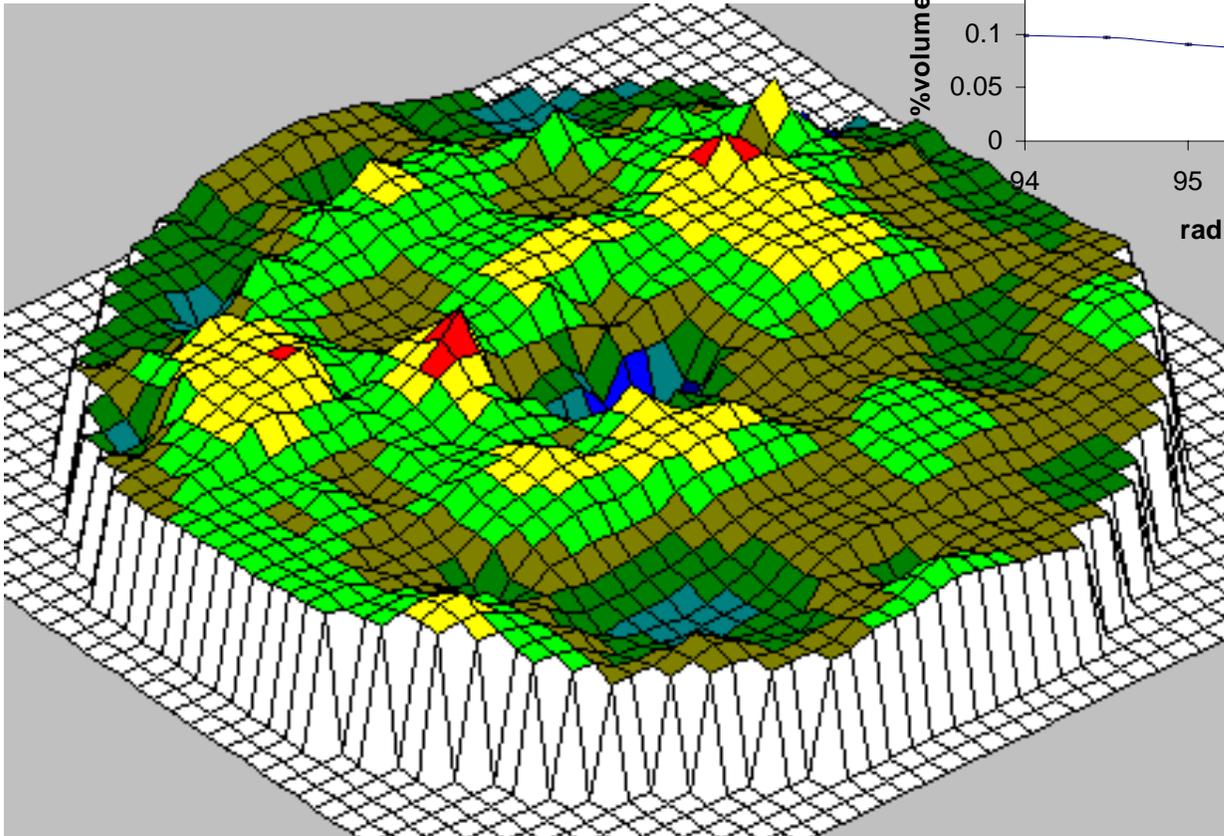
line spacing 0.27 microns





# Wafer Mapping Helps to Understand Processing Variables

Distribution of volume fraction of a (111) cyclic fiber texture on a 1micron electroplated copper deposited on 200 mm wafer (30% range of variation)



120 point map



# Summary

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- Quantitative texture analysis (QTA) has evolved as a powerful tool for material characterization
- In controlled circumstances QTA is operator independent and suitable for automation
- Application of QTA as a quality control tool is feasible; it has been proven in the sheet metal industry and is being evaluated in the semiconductor industry